



Acoustic Wave Sensors: Modes, Responses and Hydrophobicity

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www.naturesraincoats.org

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Overview

- 1. Basics of Acoustic Wave Sensors
 - Acoustic waves: Modes and devices
 - Sensing principles: Solids and liquids
- 2. Layer-Guided Acoustic Waves
 - Love waves & acoustic plate modes
 - Layer-guided devices: Operating points and sensitivity
- 3. Sensor Research Examples
 - Steroids: Molecularly imprinted polymers
 - Cancer vaccines: Peptide binding
- 4. Current Acoustics Research
 - VetAI: Sperm motility
 - Green solvents: Ionic liquids and microfluidics
 - Wetting: Hydrophobicity and slip on topographically structured surfaces

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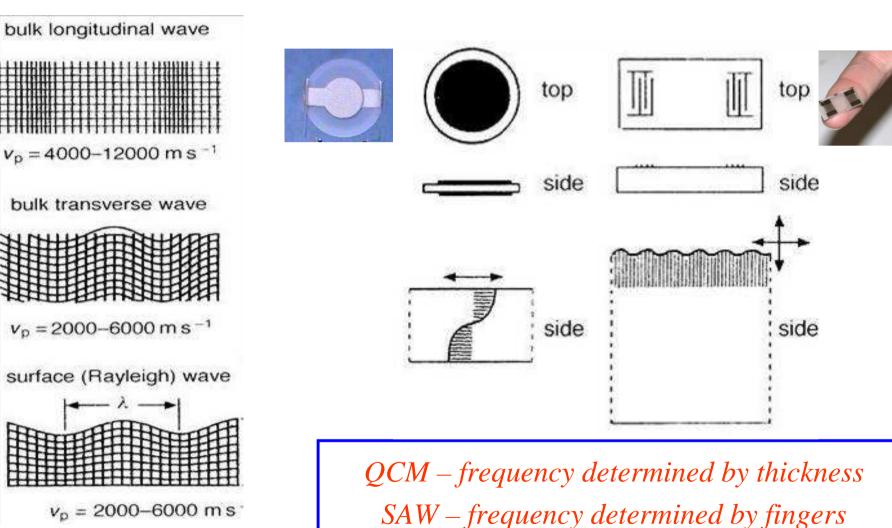
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Basics of Acoustic Waves



Acoustic Waves

Acoustic Waves

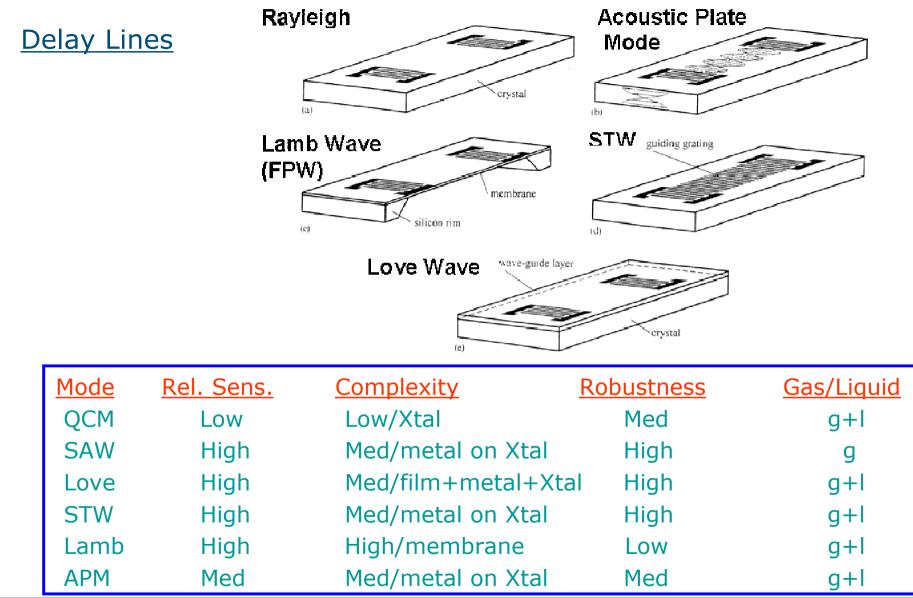


QCM

versus

SAW

Acoustic Wave Modes



QCM/QCR Sensing Principles

Thickness Shear Mode Vibration

QCM has a sharp resonance

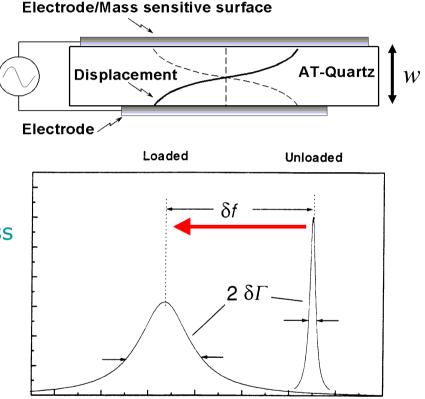
Frequency given by quartz thickness, w

 $v_s = f\lambda \implies f = 2v_s/w$

Mass Loading or Immersion

QCR resonant frequency reduces due to mass Resonance broadens due to polymer/liquid

Sauerbrey equation $\Rightarrow \Delta f \propto -f^2 \Delta m/A$ Kanazawa & Gordon $\Rightarrow \Delta f \propto -\sqrt{(\eta \rho)} f^{3/2}$



Increasing mass or viscosity-density product decreases resonant frequency
 Increasing viscosity-density product (or polymer) broadens resonance

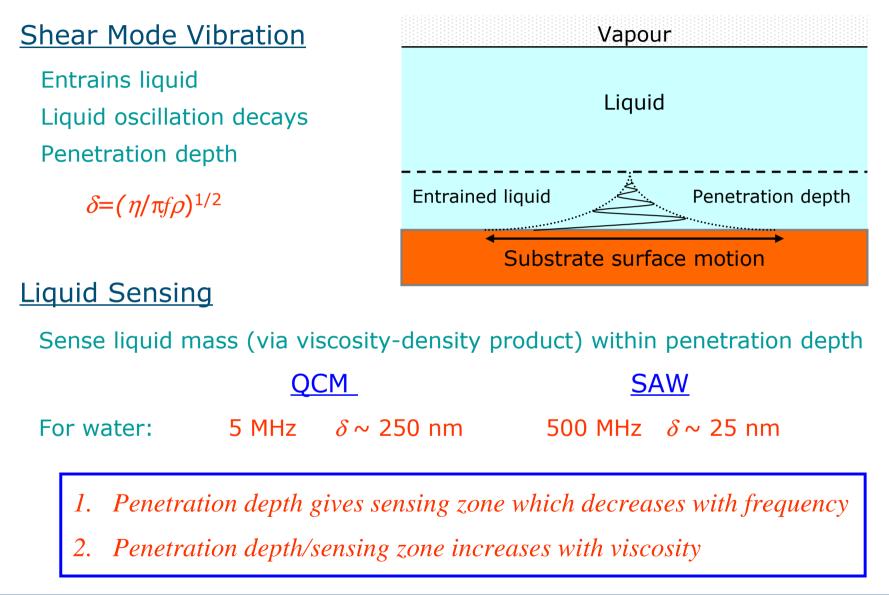
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Sauerbrey, G., Z. Phys. <u>155</u> (1959) 206-222. Bruckenstein, S; Shay, M., Electrochim. Acta <u>30</u> (1985) 1295-1300. Kanazawa, K.K.; Gordon, J.G., Anal. Chim. Acta <u>175</u> (1985) 99-105.

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Liquids and Penetration Depth





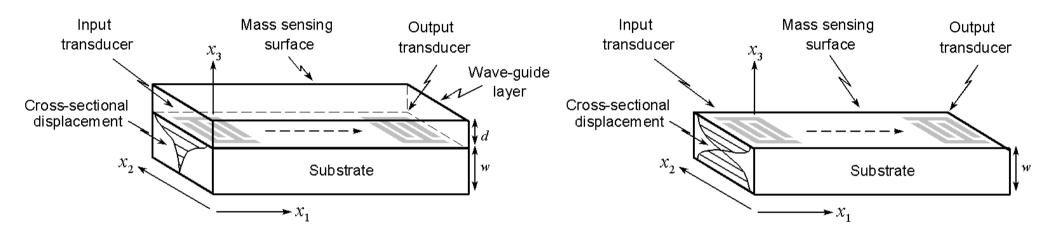
Layer-Guided Acoustic Waves



Love Waves versus SH-APMs

Love Wave

SH-APM

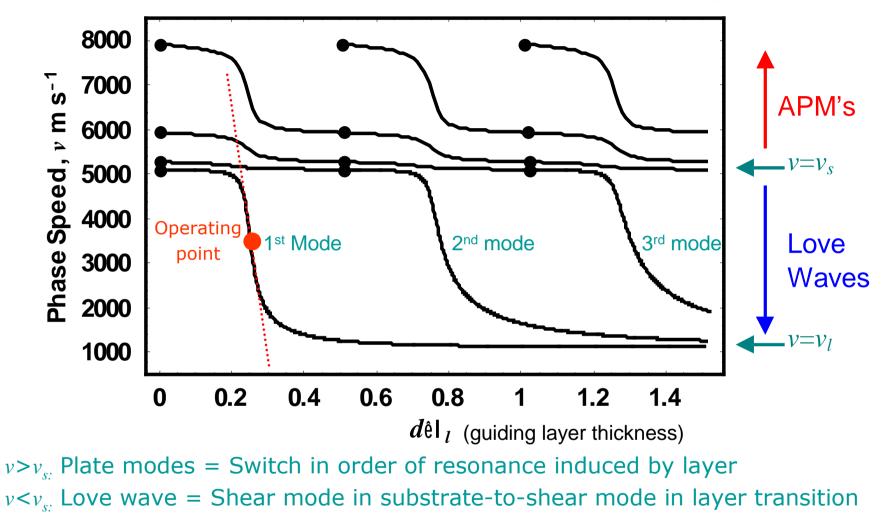


Layer guided SH-SAW with $v_l < v_s$ Surface localised wave Increased sensitivity "QCM with propagation" Substrate resonance Sensing via both faces

Increased sensitivity versus isolation between sensing face and transduction



Generalized Love Waves – Operating Point



Increased mass/liquid sensitivity related to slope of dispersion curve

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McHale, et al, J. Appl. Phys., 2002, <u>91</u>, 5735-5744; 9701-9710.

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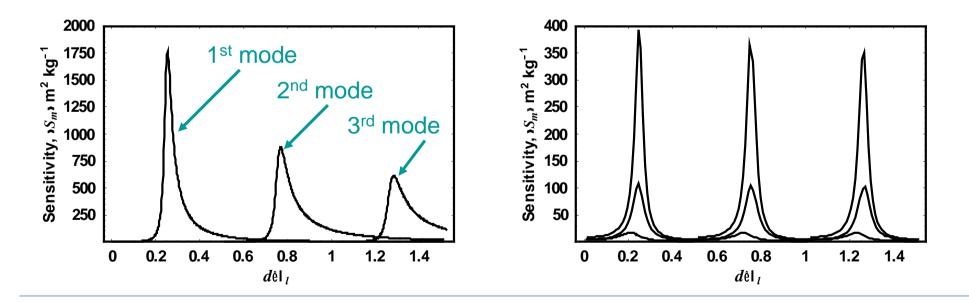
Phase Speed Mass Sensitivity

$$S_m = \lim_{\Delta m \to 0} \frac{1}{\Delta m} \left(\frac{\Delta v}{v_o} \right) \approx \frac{f_o}{\rho_l v_l} \left(\frac{d \log_e v}{dz} \right)_{z_0}$$

 Δm is mass per unit area being sensed, $z=df/v_l$ is the normalized thickness "Rigid" mass \Rightarrow Mass sensitivity is slope of dispersion curve

Love Waves

Layer-Guided SH-APMs

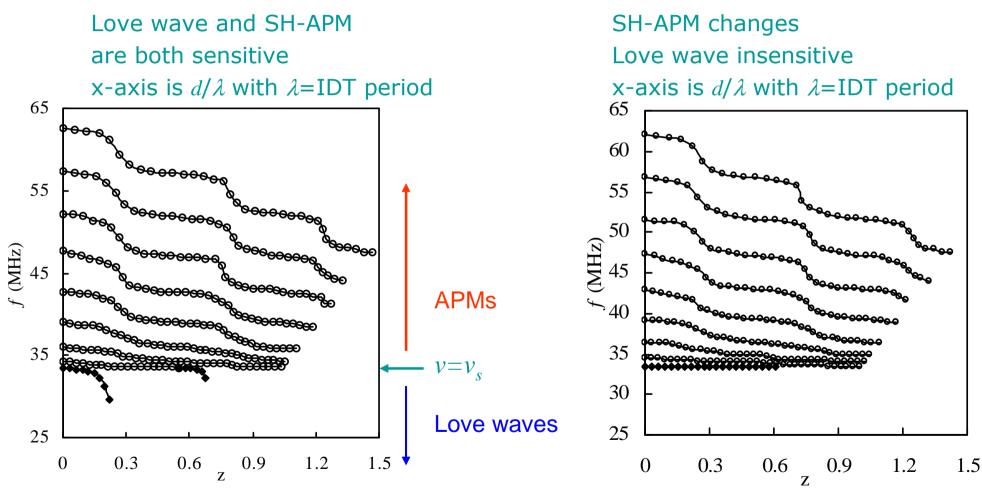


Experimental Data for Layer-Guided SH-APMs

25 MHz surface skimming bulk wave (SSBW)

Propagation orthogonal to x-axis of thinned (200 mm) ST-Q substrate

IDT Face Coated



McHale, et al, Appl. Phys. Lett., 2003, 82, 2181-2183.

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Newton, *et al*, *Sens. Act.*, 2004, <u>A109</u>, 180-185. F. Martin, PhD Thesis, Nottingham Trent University (2002). 12 NTU

Opposing Face to IDTs Coated

Generalized Sauerbrey/Kanazawa & Gordon

Polymer Waveguide on Polymer Substrate

Complex velocity shift

$$\frac{\Delta v}{v_o} \approx \left(\frac{1 - v_f^2 / v_o^2}{1 - v_l^2 / v_o^2}\right) \left(\frac{d \log_e v}{dz}\right)_{z=z_o} \left(\frac{\tan\left(T_f^o h\right)}{T_f^o h}\right) \frac{\omega \rho_f h}{2\pi v_l^\infty \rho_l} (\rho \eta \omega)^{1/2}$$
Complex slope factor from polymer waveguide

tanx/x factor gives mass/liquid loading limits

$$\left(\frac{\tan\left(T_{f}^{o}h\right)}{T_{f}^{o}h}\right) \rightarrow \begin{cases} 1 & h \to 0 & \text{Sauerbrey/solid limit} \\ \frac{-\sqrt{-2j}}{2h\left(1-v_{f}^{2}/v_{o}^{2}\right)}\sqrt{\frac{2\eta_{f}}{\omega\rho_{f}}} & h \to \infty \text{ and } \omega\tau \to 0 & \text{Kanazawa \& Gordon/liquid limit} \end{cases}$$

Sensor Research Examples (Selected) Past Work

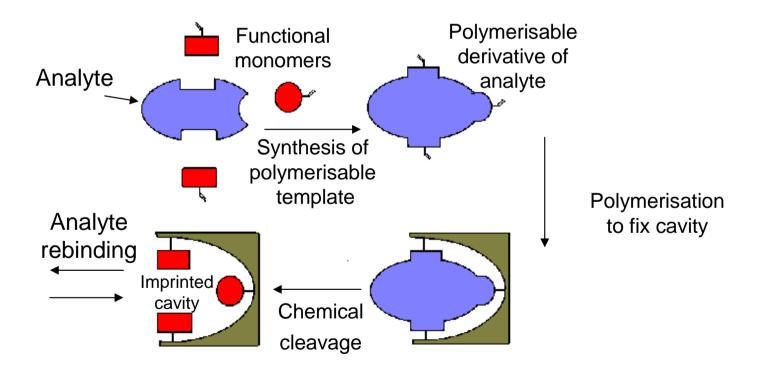


Example 1: Steroids and MIPs

Target Applications (Liquid Phase)

Recognition/selectivity via molecularly imprinted polymers (MIPs) Applications: monoterpenes, amino acids, *topical steroids* Tailor made enantioseparation materials

MIP - Polymer Type Artificial Receptor





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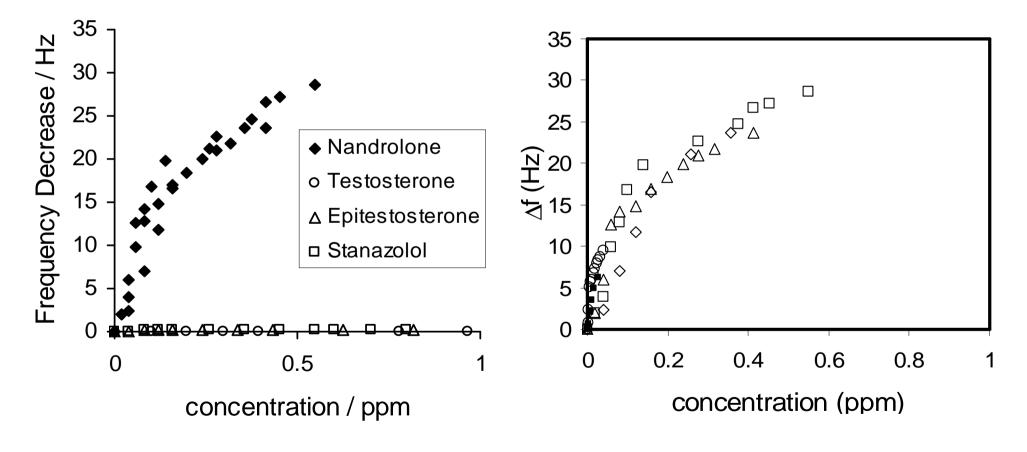
Selectivity to Nandrolone

QCM Coating

Spin coated/cast layer Covalent imprinting strategy

Response to Replicates

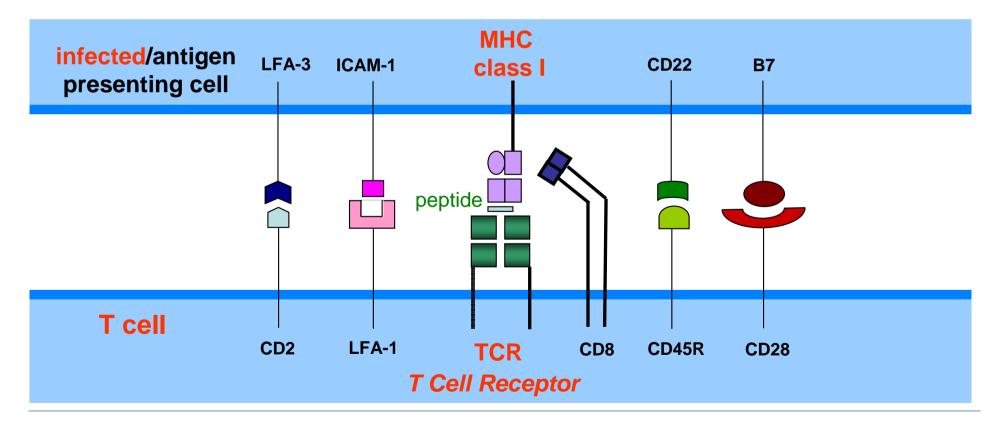
One-shot screening Test data for 5 crystals





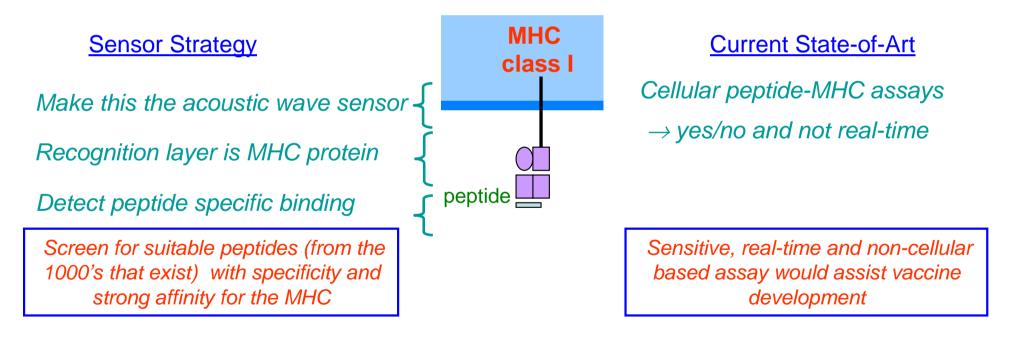
Example 2: Vaccines - Peptides and T-Cells

- 1. Infection/virus broken into peptide fragments and presented on cell surface
- 2. Cytotoxic T-cells attach to peptides and "read" peptide sequence
- 3. If foreign, cell is killed by release of a cytotoxic chemical
- 4. Major histocompatability complex (MHC) antigens are responsible for the expression of peptides on the infected cell
- 5. Vaccine introduces peptide to the T-cell Aim is to find suitable peptides

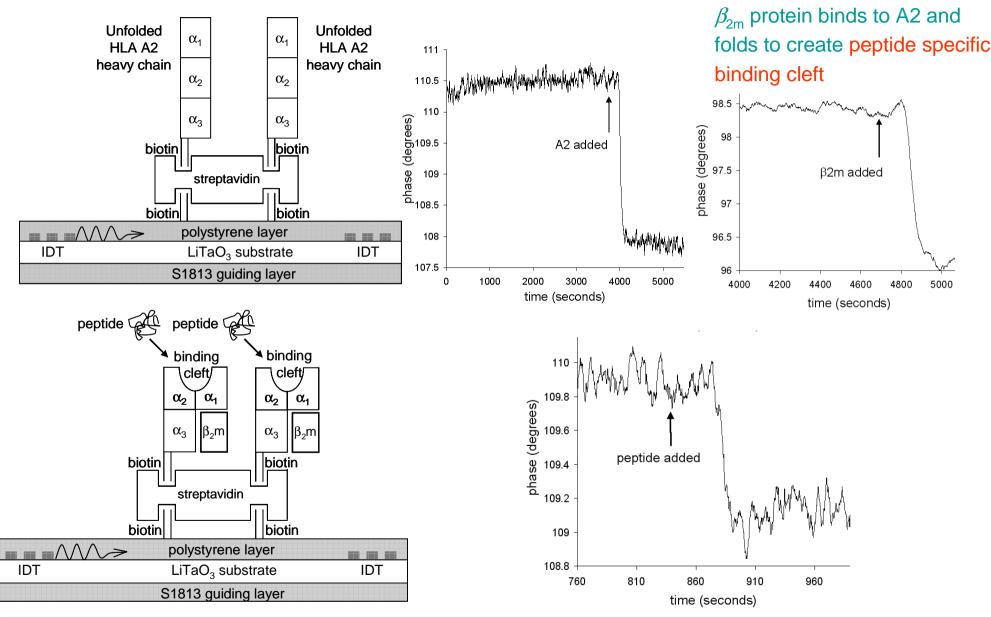


Peptides and T-Cells

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Flow Cell with Love Wave Screening Device



Stanley, et al, Analyst, 2006, 136, 892-894.

Acoustic Wave Research Current Sensor Work



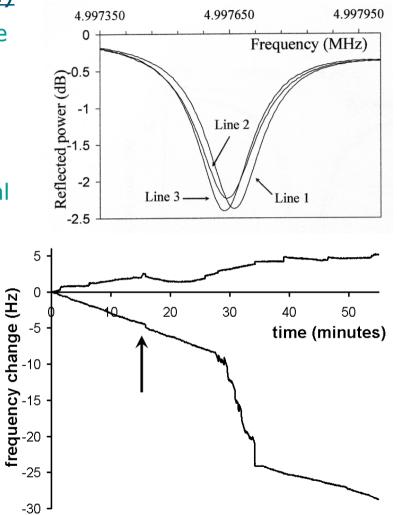
Project 1: Sperm Motility

Veterinary Artificial Insemination (VetAI)

- Sperm Quality Assessment & Detection Device (SQuADD)
- Time of flight/swim
- 5 MHz QCM (or use other AWS device)
- Frequency drop relative to reference
- Crystal pre-coated with sperm 'sticky' material

Experimental Sequence

Stabilisation of signal in PBS Addition of sperm (arrow) Time of arrival data – swim speed





Project 2: Ionic Liquids Chip

Determining Physical Properties

Room temperature ionic liquids (RTIL's) Green because non-volatile Millions of simple IL's, billions of binary ILs, ... Designer solvents Poorly characterised

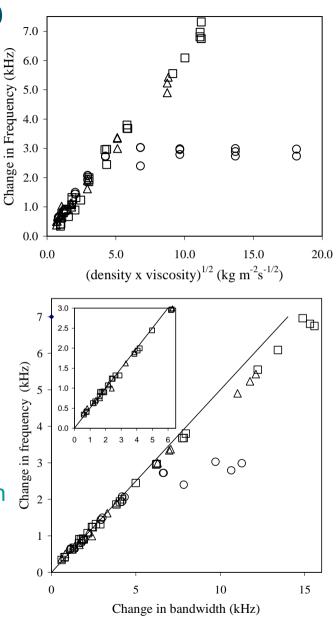
<u>QCM</u>

Can measure density-viscosity product, but can also determine whether Newtonian via coupled frequency shift-bandwidth increase

 $\Delta f = -\Delta B/2$

<u>Data</u>

Polydimethylsiloxane oil - known non-Newtonian at higher molecular weights (ooo) Two ionic liquids $[C_4 mim][OTf] (\Box \Box \Box)$ and $[C_4 mim][NTf_2] (\Delta \Delta \Delta)$



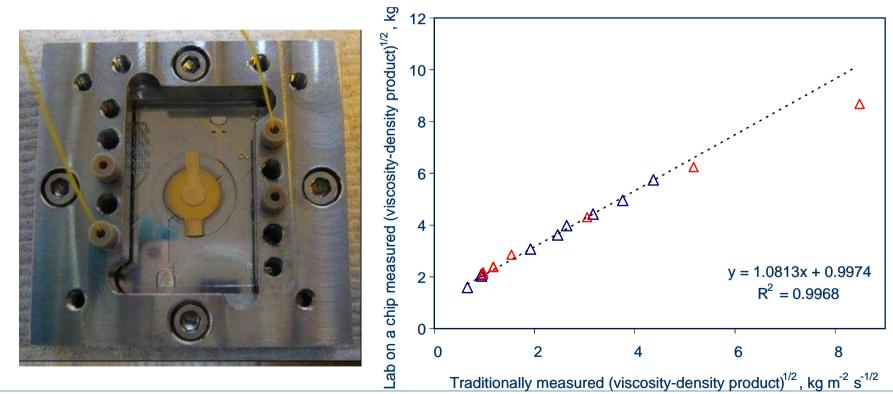
McHale, *et al, Anal. Chem.*, 2008, <u>**80**</u>, 5806-5811. Ge, *et al, Anal. Chem.*, 2009, <u>**81**</u>, 1628-1637.



Chip Version – Dilutions of Ionic Liquids

Experiment

- Sample: 30 μl with 10 μl in contact with QCM
- QCM: 14 mm diameter, rough surface, 10 MHz operated at 3^{rd} harmonic (30 MHz) Flow-rate: 0.06 µl/s
- Liquids: Glycerol/water and [C₄mim][NTf₂]/methanol
- Also looked at smooth QCMs and pure ILs

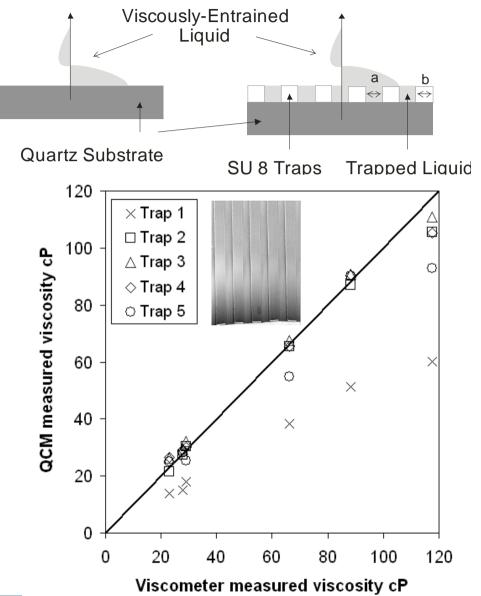


Separating Viscosity from Density

Original Concept (Martin et al)

Dual QCM: Smooth and trap surfaces Frequency shifts allow separation of viscosity from density Our traps are fabricated using SU-8 Various ionic liquids used Currently off-chip results

Тгар	Width μm	Separation μm	Effective Height μm
1	10.7	30.4	0.838
2	24.1	34.5	2.118
3	43.3	52.5	1.818
4	70.5	84.0	1.419
5	108.0	97.0	1.277

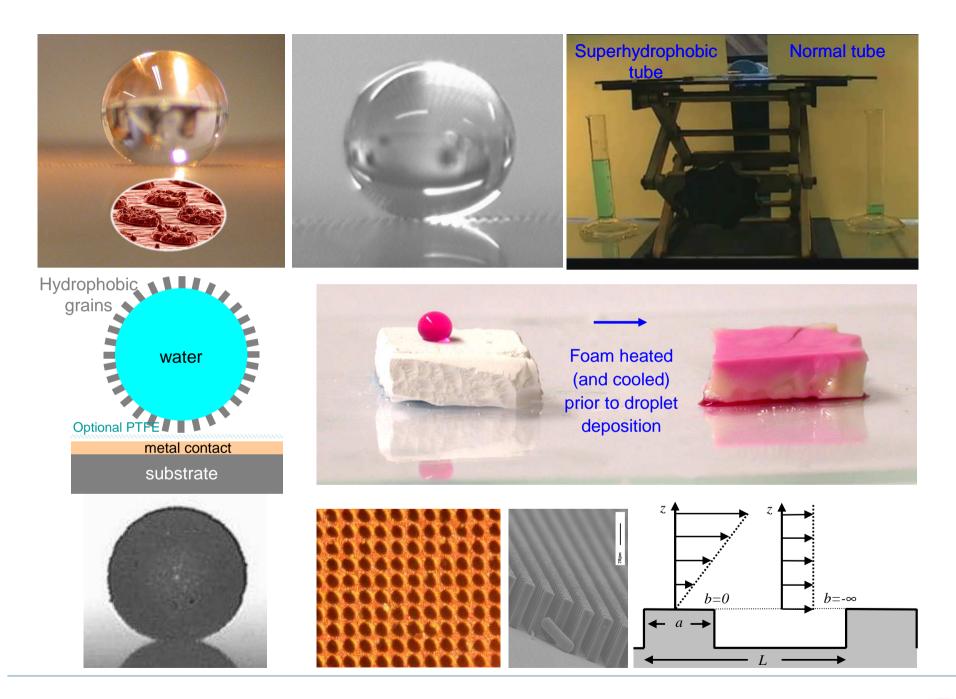


Martin, *et al*, *Sens. Act A*, 1994, <u>44</u>, 209-218. Doy, *et al*, *IEEE Sensors Conference* 2009.



Acoustic Wave Research Wetting and Acoustics Work

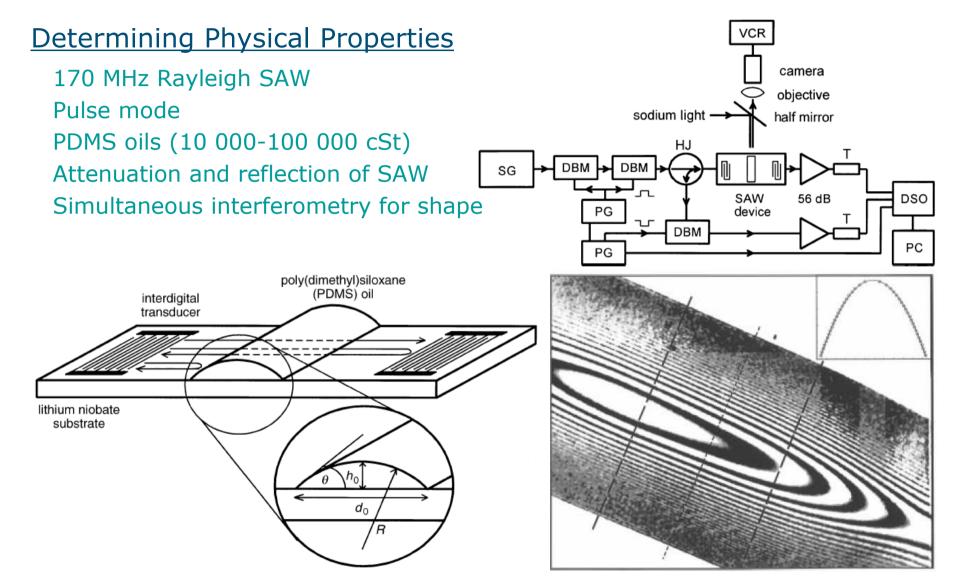




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Old Work: SAWs and Stripes of Oil

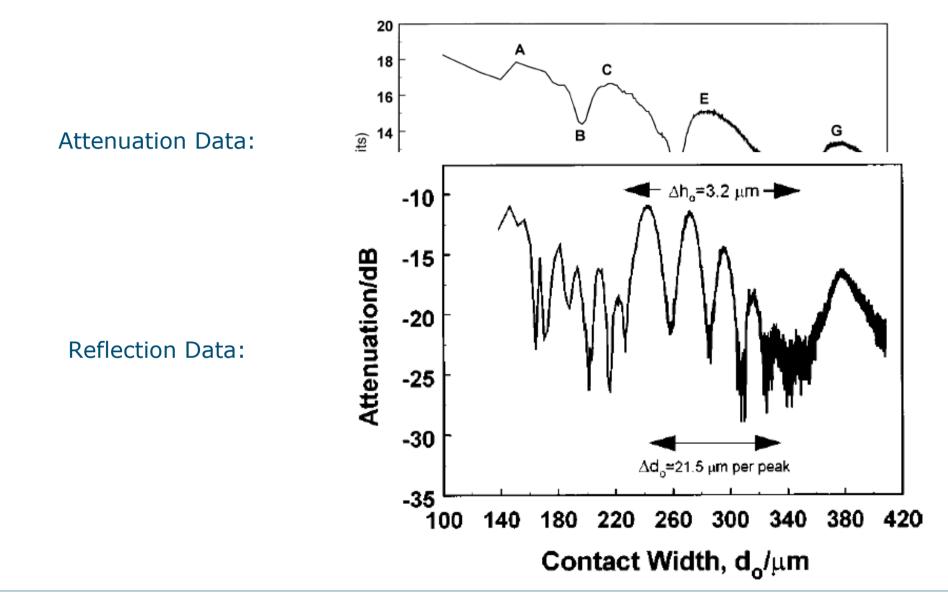


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 McHale, et al, Faraday Discuss., 1997, 107, 15-26; Phys. Rev.. B. 1998, ???
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 McHale, et al., Appl. Phys. Lett. 1997, 71, 3785-3786
 3785-3786



Old Work: Attenuation and Reflections



McHale, *et al, Faraday Discuss.*, 1997, <u>107</u>, 15-26. McHale, *et al.*, *Appl. Phys. Lett.* 1997, <u>71</u>, 3785-3786

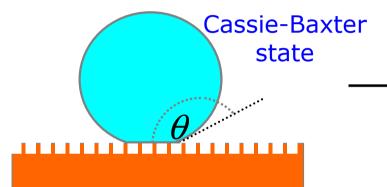


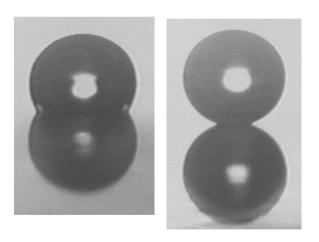
Current Work: Superhydrophobicity

Immersed Superhydrophobic Surfaces

Provided design of features correct, penetration of water can be resisted

A silvery sheen can be seen when immersed – due to surface retained layer of air.







Hydrophobicity and Acoustics

What <u>might</u> happen when an acoustic wave device has a hydrophobic, or a structured hydrophobic or even a superhydrophobic surface?



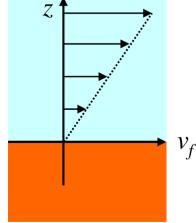
Usual Hydrodynamic View of Acoustic Response

Mathematical Formulation

Wave equation for substrate and solid layer or Navier-Stokes equations for liquid define substrate and layer/fluid displacementsMatch solutions at boundary (substrate-air, substrate-layer or substrate-liquid)Provides dispersion equation and solution gives resonances

No-Slip Boundary Condition

Solid-Air	\Rightarrow	$q_s(z=0)=q_l(z=0)$	substrate & layer displacements
			match at all times
	i.e.	$v_s(z=0)=v_l(z=0)$	speeds at wall match
Solid-Water	\Rightarrow	$v_s(z=0)=v_f(z=0)$	speeds at wall match - fluid
			speed extrapolated from bulk



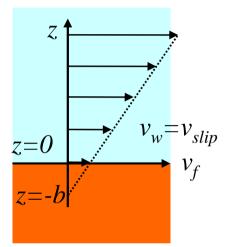
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The Effect of Wall Slip: Theory

Flow Profile

With slip length, *b*



<u>Equations</u>

Match speeds

$$v_s(z=0) = v_f(z=-b)$$

Expand

$$v_w - v_f (z = 0) = -b \left(\frac{\partial v_f}{\partial z}\right)_{z=0}$$

Slip length, *b*, models effective position of interface Negative *b* implies effective interface moves to liquid side of boundary Force exerted on wall divided by viscosity

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Slip length is a mechanism for modelling an effective average boundary and/or taking into account liquid-solid interfacial forces

McHale, et al., *J. Appl. Phys.*, 2000, <u>88</u>, 7304-7312; 2004, <u>95</u>, 373-380. Ellis, J. G., *et al.*, *J. Appl. Phys.*, 2003, <u>94</u>, 6201-6207.



Effective Sauerbrey "Trapped Liquid Mass"

Equations of Motion

Solve with slip boundary condition for acoustic impedance Consider in terms of slip length and interpret solution for small *b*

Newtonian Liquid

Kanazawa & Gordon result for no-slip modified by "slip" correction using b/δ

Negative Slip Length

Define a liquid mass as $\Delta m_f = b \rho_f$

$$\left(\frac{\Delta\omega}{\omega}\right)_{slip} \approx \left(\frac{\Delta\omega}{\omega}\right)_{no\ slip} \left(1 - \frac{2b}{\delta}\right)$$

Slip length to penetration depth ratio

 $Z_L^{slip} \approx \frac{Z_L^{no \, slip}}{1 + \frac{b}{m} Z_L^{no \, slip}}$

$$\left(\frac{\Delta\omega}{\omega}\right)_{additional} \approx \left(-\frac{2b}{\delta}\right) \left(\frac{\Delta\omega}{\omega}\right)_{no\ slip} = \frac{\omega \Delta m_f}{\pi \sqrt{\mu_s \rho_s}}$$

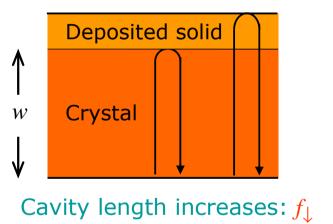
Kanazawa & Gordon viscosity-density product contribution + trapped "Sauerbrey-like liquid mass", <u>but</u> this assumes all locations are equal, i.e. complete liquid penetration.



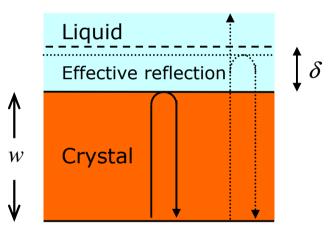
Implicit Assumptions: Acoustic Reflection View

Simple Cavities and Standing Waves

- Solid-Air \Rightarrow Uniform and strong reflection
- Solid-Water \Rightarrow Partial reflection at an effective plane within penetration depth







Cavity length increases: f_{\downarrow} Reflection becomes partial: B_{\uparrow}

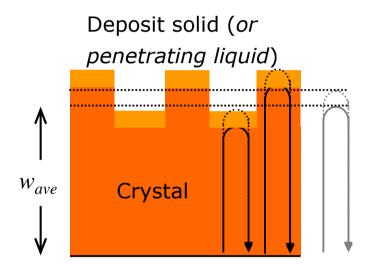
Assumes reflection from all locations along the surface are of equal strength



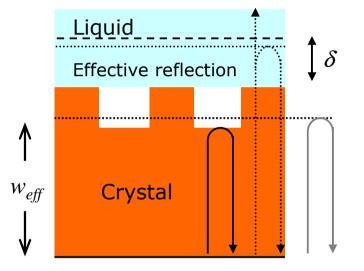
Effect of Topography and Hydrophobicity?

Structured Cavities and Standing Waves

- Air contact \Rightarrow Equally strong reflections from peaks and troughs of surface
- Water contact \Rightarrow Changes cavity length and strength of reflection defined by peaks



Effective cavity length Peaks and trough increase cavity lengths equally: f_{\downarrow}



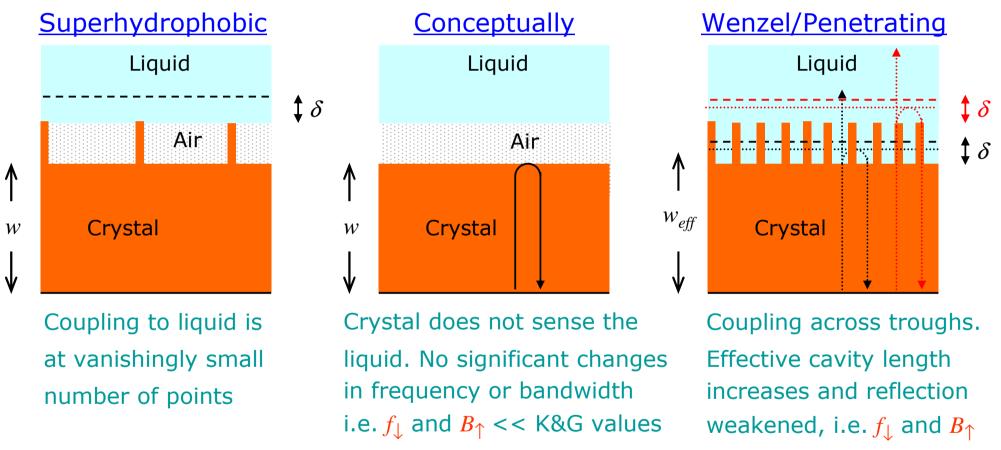
Effective cavity length increased? i.e. f_{\downarrow} Or top reflection weakened? If lower cavity length becomes dominant: f_{\uparrow}

Skating form of superhydrophobicity offers possibility of new liquid phase responses

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Extreme Superhydrophobic Case

Water immersion \Rightarrow Water skates across surface features and pressure (or other force) is needed to force capillary penetration

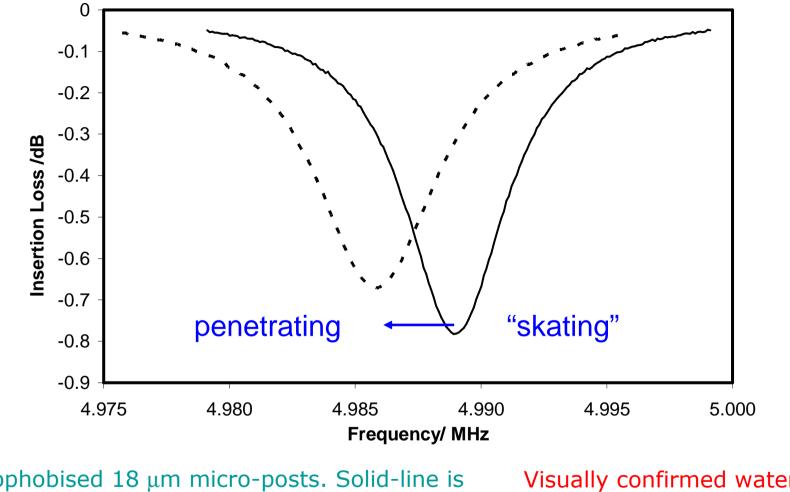


QCM behaves as if decoupled from the liquid, unless liquid penetrates into structure

McHale, G.; Newton, M.I., J. Appl. Phys., 2004, <u>95</u>, 373-380.

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QCM with Microposts: "Skating" Transition

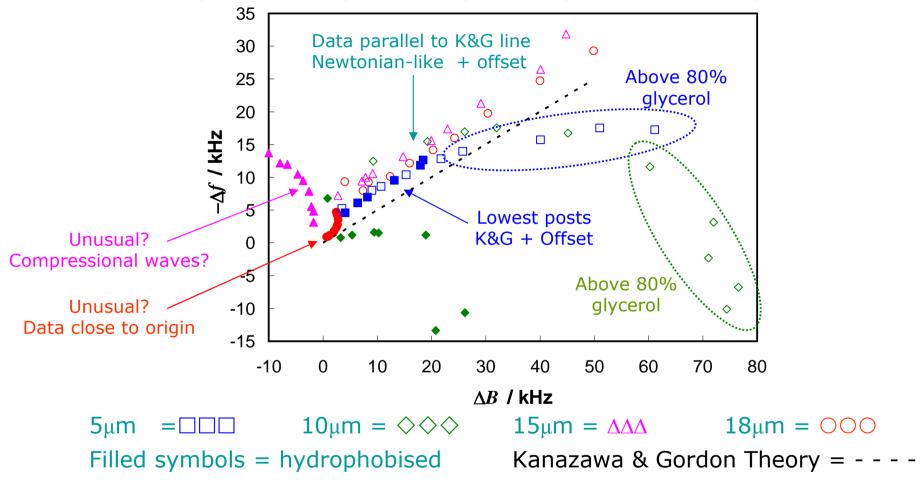


Hydrophobised 18 μm micro-posts. Solid-line isVisBefore pressure applied. Dotted curves is afterafpressure is applied.

Visually confirmed water ingress after pressure applied

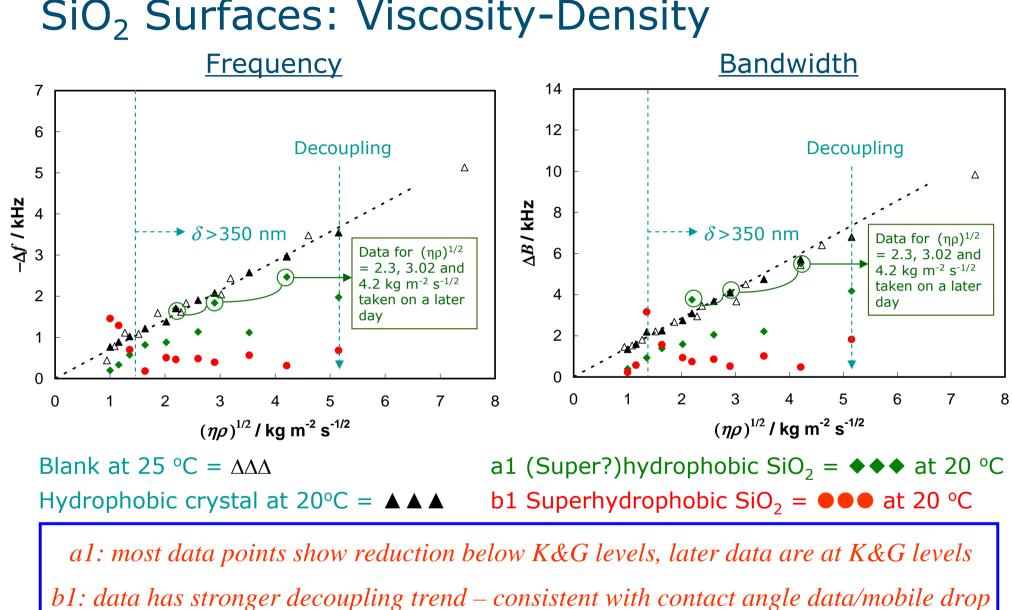
Micro-Post Surfaces – Water/Glycerol Mixtures

Bare (non-hydrophobised) and Hydrophobised (0-100%)



Hydrophobisation of posts changes type of response – all data generally closer to origin





SiO₂ Surfaces: Viscosity-Density

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Conclusions

- 1. Acoustic Wave Devices
 - Many modes for liquid and gas phase operation
 - Well established as effective sensors in simple systems
- 2. Current Research on Sensors
 - Sperm motility using simple swim time and effective "mass"
 - Lab-on-a-Chip for ionic liquids + traps to separate viscosity
- 3. Hydrophobic Surfaces
 - Response depends on combination of topography and hydrophobicity
 - "Slippy" superhydrophobic surfaces should decouple acoustic response
 - Skating-to-penetrating transition could be used as a sensor principle

The End



Acknowledgements

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